# 10.000 DWT Coal Vessel/Barge Open Pier Jetty Planning at Molotabu, Gorontalo

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Abstract—Coal exports and imports are common in Indonesia, especially Gorontalo, North Sulawesi, which is always involved in coal export and import activities. Coal is one of the important energy sources in this country. These activities always involve ships. A ship certainly needs a station like any other form of transportation. Open pier construction has various regulations so that vessel can dock safely. Various things can affect the dimension and even the strength of the port structure. From the planning of the pier, implementation methods are also carried out to calculate the planned cost budget The results of planning an open pier jetty for a 10,000 DWT barge include a minimum depth recommendation of -6.5 mLWS. Recommended jetty dimensions are 108 m long and 20 m wide at an elevation of +2.5 mLWS. From the results of the upper structure calculations, a plate with a thickness of 35 cm was obtained. Then for the beam requirements for the jetty structure (500 x 750 mm) and fender beams (2600 x 2500 x 1200 mm). For single pile cap required  $(2000\ x\ 2000\ x\ 1000\ mm)$  and batter pile cap  $(3000\ x\ 2000\ x\ 1000$ mm). From the results of the substructure calculations, it was found that D609 mm steel piles with a thickness of 12 mm were needed for the jetty structure. Dredged volume requirement is 20,300 m3. Breast wall dimensions (400 x 2000 mm), cantilever dimensions (150 x 250 mm), foot dimensions (2500 x 400 mm), and stiffener thickness of 30 cm. From the overall calculation results, the implementation method can be planned as follows. Preparatory work, dredging work, retaining wall work, jetty structure work, and fender and bollard installation work. From this work, the total cost required is Rp. 51.324.256.809.

Keywords-Cost Estimating, Dredging, Jetty, Open Pier, **Retaining Wall.** 

# I. INTRODUCTION

**♦**OAL is Indonesia's most vital mining commodity. One form of utilization of coal is as a source of energy for power generation. Indonesia itself is one of the largest thermal coal producers and exporters in the world. Based on the Ministry of Energy and Mineral Resources website, Indonesia has coal resources of 143.7 billion tons. The availability of such large natural resources of coal can provide its own advantages, especially if the raw minerals are processed domestically. Therefore, the presence of coal is still very much needed in Indonesia, considering that this fossil fuel provides many benefits for humans.

To support the potential of Gorontalo and its surroundings which have many advantages because it is close to the Philippines and international traffic (sea transportation) is quite busy. Besides, the potential in the fields of industry and trade is racing against each other in the economic development of the Manado-Bitung Integrated Economic Development Zone (KAPET). However, these developments must be accompanied by the availability of adequate electricity.

In order to fulfill as well as to support the rapid development of the waters in Gorontalo and its surroundings,



Location of project

for 10.000 DWT coal barges at Molotabu, Gorontalo, as operational fuel for the Power Plant must be carried out and the design based on [1-13].

#### II. RESEARCH METHOD

#### A. Location of Research

The location of this jetty planning is in the North of Sulawesi, Molotabu, Gorontalo, with the detail of location can be seen on Figure 1.

#### B. Flow Chart

Flow chart of this planning can be seen on Figure 2.

C. Collecting and Data Analysis

Collected data analyzed based on [1].

# 1) Tides Data

Phenomenon of periodic ups and downs of sea levels caused by a combination of gravity and the attractive force of astronomical objects, especially the sun and the moon on the earth. The tides data result can be seen on Table 1.

#### 2) Bathymetry Data

Bathymetric maps are maps that show contours seabed depth from the position of 0.00 mLWS. Bathymetry map at Molotabu, Gorontalo, can be seen on Figure 3.

From the results of observing currents around the location, the maximum current speed is 0,5 m/s



Figure 2. Flowchart.



Figure 3. Bathymetry map.

# 3) Wind Data

Wind data can be seen on Table 2

# 4) Wave Data

Wave data obtained with several steps. Firstly, forecasting based on wind data and fetch effective, and the outcome is wave height each wind direction. Second, analysis with Weibull and Gumbel method in order to find wave height in 2, 5, 10, to 100 years return period. Last, from each data, we took the most critical value and R value close to 1, and then analyze with refraction considerations due to seabed elevation difference to gain wave height on the face of the jetty. Based wave analysis, the wave height taken is +1,76 mLWS.

# 5) Soil Data

Soil data used for this project based on 2 points of bore log. Named BL-1 and BL-2. SNI 1726:2020 is used for determining the classification of the soil. Soil data can be seen





Figure 5. 10.000 DWT coal barge.





2.75 m



# on Figure 4.

# 6) Vessel Data

The specification of the vessel is shown below:

- a. Dead Weight Tonnage (DWT) = 10000 MT
- b. Length of Overall (LOA) = 96,56 m
- c. Breadth (Width) = 27,43 m
- d. Draft = 4,88 m
- e. Depth = 6,1 m

The designed vessel can be seen on Figure 5.

# 7) Unloading Equipment

The equipment used for unloading purposes is truck. The specification and dimension of the truck is based on SNI



	/	,	,	,				
2008	4,62	6,78	4,34	3,33				
2009	4,50	7,52	4,77	3,55				
2010	5,53	5,18	3,63	4,07				
2011	4,70	6,91	3,96	4,18				
2012	4,80	6,74	4,42	3,47				
Max	5,53	7,90	5,33	5,04				
		Tabl	le 3.					
	]	Moment of Slab	Recapitulation					
Туре		Position	Moment	(kg.m)				
		Mlx	10983,9	8				
A 1		Mtx	-11327,7					
AI		Mly	13823,51					
		Mty	-17049,97					
		Mlx	780,48					
12		Mtx	-780,48					
AL		Mly	780,48					
		Mty	-780,48					
		Mlx	1860,31					
12		Mtx	-2419,82					
A3		Mly	760,8					
		Mty	-6398,38	3				

Table 1. Tides Elevation

Symbol

HWS

MSL.

LWS

Southeast

7,07

6,92

6,42

6.54

7,72

7.33

Table 2. Wind Velocity at Molotabu, Gorontalo Recapitulation

Wind Velocity (m/s)

South

4,86

4,47

4,55

4.46

4,59

4.56

Figure 9. Jetty model in SAP2000.

1725:2015. The dimension and loads each axle can be seen on Figure 6.

#### **III. RESULTS AND DISCUSSION**

#### A. Layout Evaluation

Layout evaluations is needed for vessel can berth safely. Water layout determined, while land layout determined based on [2], [8-9].

#### 1) Water Layout

The result of water layout including; entrance channel, turning basin, berth basin, and anchorage area can be seen on Figure 7.

#### 2) Land Layout

After analyzed data, the jetty dimension is  $108 \times 20$  m. The retaining wall needed is along the jetty's length. And for dredging, the area is  $20.300 \text{ m}^3$ . The selection of heavy equipment for dredging, suction cutter is the selected heavy equipment based on seabed and volume of dredging. Figure 8 is the illustration of the selected heavy equipment for dredging. The result of land layout including; the dimension of jetty, elevation of jetty, dredging volume, can be seen on Figure 8.

#### 3) Structure Planning

Water Level Condition

West

3,66

4,84

5.26

3.97

4,55

4.60

High Water Springs

Low Water Springs

Mean Sea Level

Year

2002

2003

2004

2005

2006

2007

Structure planning designed based on [3], [5], [7-13]. For reinforcement calculation, analyzed based on [8]. Structure planning including; structure modelling, slab planning, beam planning, pile cap planning, and foundation planning. The control that must be considered is the control of the crack width. To control crack width, Equation 1 below is used.

$$W = \alpha \left( C_3 x d + C_4 \frac{dp}{\omega p} \right) \left( \sigma_a - \frac{C_5}{\omega p} \right) 10^{-6}$$

#### 4) Structure Modelling

Structure planning is started from modelling assisted by SAP2000 and the model can be seen on Figure 9.

# 5) Slab Planning

There are 3 different dimensions of slab that analyzed. The Table 3 is the moment recapitulation of each slab. Slab planning results such as reinforcement and crack control can be seen on Table 4.

#### 6) Beam Planning

In this project, there are 2 type of beam. The difference is only on the beam's span, 8 m span and 2 m span. Table 5 is the recapitulation of beam's moment. Beam planning results

Elevation (mLWS)

Southwest

3,91

4,09

3,53

4.11

3,97

4.69

+1,343

+0,671

0.00

				Flex	ural R	einfo	rcem	nent and	d Cr	ack (	r. Contr	ol in S	lab Re	ecapi	tulatio	on						
Type	Lengtl	n Width	Thick	kness							Fle	kural F	Reinfor	rcem	ent						- Cray	ok Control
Type	(mm)	(mm)	(mm)	)	Sup	port X	ζ		Su	pport	Y		Fie	eld X			Fie	ld Y			Cla	K COIIIIOI
A1	8000	8000	350		D	22	-	125	D	22	-	90	D	22	-	125	D	22	-	100	OK	
A2	2000	2000	350		D	16 16	-	125	D	16	-	125		16	-	200		16	-	200	OK	
AS	2000	2000	330		D	10	-	200	D	10	-	123	D	10	-	200		10	-	200	UK	
							Mo	ment of	Ta f Be	able 5 am R	i. lecap	itulatio	on									
Туре						Fo	orce					I	Mome	nt (kl	N.m)							
B1						M	ltum					-	557,69	9								
						M	llap [tum					-	399.4									
B2						M	llap					3	38,03									
Diania E	· · · · · ·					Μ	ltum					-	1826,8	8								
Plank F	ender					Μ	llap					1	826,8									
					<i>c</i>				Ta	able 6	<b>5</b> .											
				Rein	forcer	nent I	Need	ed and	Cra	$\frac{\operatorname{ck} C}{c}$	ontro	ol in Be	eam R	ecapi	tulati	on	D					
Type		Length	Height	Width	C	+	Fl	exural	Ren	nforce E:-1	emen	it		C.		Sh	ear Re	inforc	eme	nt		Crack
D1		(mm) 8000	(mm) 500	(mm) 750	 	port	D	40		Field	1	D	40	SL	12	l .	200	Fl	12		200	OK
B1 B2		2000	500	750	4	-	D	29		2	2	D	29	ø	13	-	150	ø	13	-	150	OK
Plank F	ender	2000	200	150	D	36	-	100	)	Đ	36	-	100	ø	13	-	150	ø	13	-	150	OK
						Ν	Mom	ent of	Ta Pile	able 7 Cap	'. Reca	pitulat	tion									
Туре						Р	ositi	on						Mor	nent	(kg.m)	)					
~						N	Лx							2924	42.51							
Single l	Pile Cap					Ν	Лy							579	97,49							
Batter I	Pile Can					Ν	Лx							8793	32,76							
Datter	ne Cap					N	Лу							914:	57,83							
				Flexur	al Rei	nforc	emei	nt and (	Ta Tac	able 8	3. Introl	in Pil	e Can	Reca	nitula	tion						
Type		Length (mm)	W	idth (mm	)	Thi	ckne	ess (mn	n)		Flex	ural R	einfor	ceme	nt					(	Crack C	ontrol
2 F -	-	- <u>-</u> )		(	,			(	/					2	K-Dir	ection			Y	-Dire	ction	
Single		2000	20	00		100	0				D	32	-	20	)	D	32	-	100	) (	OK	
Batter		3000	20	00		100	0				D	40	-	12:	5	D	40	-	140	) (	OK	
								1.5.	Ta	able 9	). D	•, •										
		_				L	Jesig	gned Pi	ie D	eptn	кеса	ipitula	uon					P		G	•.	
Туре		Force	D.''	<i>(</i> , )	Mo	ment			<i>.</i>			Pile D	epth (1	n)				B	earin	g Cap	acity	4.55
Circ -1 - 1		Push (ton)	Pull	(ton)	M	$\frac{1}{500}$	.m)	My	$\frac{1}{5.02}$	n.m)			- `	17				Pı	ill (k	N)	Push	(KN)
Single I	rile (PI)	10/,54	-	12	2	3,08 4 99		2	3,92 2 14	2 5				1/	8-2				- 710/	14	49 25	23,18 21.57
Single 1	File (D7)	134,01	24,	,42	5	4,00 1 82		2	∠,40 5 2	J				11	ασ				/10,4	+-+	30	01,07 01/13
Single	инс (Г <i>2</i> )	139,17	-		5	+,00		3	5,5					15					-		40	71, <del>4</del> 3

Table 4

such as reinforcement and crack control can be seen on Table b. Mo 6.

# 7) Pile Cap Planning

2 types of pile cap is planned in this project, for single pile and batter pile. Because the unloading process using truck, there are eccentricity need to be considered. Table 7 is moment recapitulation on pile cap. Pile cap planning results such as reinforcement and crack control seen on Table 8.

# 8) Foundation Planning

There are several control need to be analyzed including; bearing capacity analyzis, depth of pile (Table 9), strength of pile control (Table 10), and reinforcement of pile (Table 11). Strength of pile control equation is shown as equation (2)-(8) below.

a. Deflection Control

c. Axial Control

$$F_e = \frac{\pi^2 E}{\left(\frac{KL}{r}\right)^2}$$

d. Axial - Moment Interaction Control

$$\frac{P_U}{P_n} + \frac{8}{9} \left( \frac{M_{ux}}{M_{cx}} + \frac{M_{uy}}{M_{cx}} \right) \le 1$$

e. Tension Control

$$\sigma < \sigma_{allow}$$

f. Shear Control

$$V_{\mu} < 0,75 V_{r}$$

g. The Ability of The Pile to Stand Alone

Strength of Pile Control Recapitulation										
Domork		Jetty								
Remark	Existing	Allowable	Status							
Deflection Control (mm)	14,9	25	OK							
Moment Control (ton.m)	25,92	86,13	OK							
Axial-Moment Interaction Control (ton)	167,54	483,9	OK							
Shear Control (ton)	6,68	403,25	OK							
Tension Control (Mpa)	74,61	284	OK							
The Ability of The Pile to Stand Alone (s)	0,36	3,15	OK							

	Table 11.															
	Reinforcement Needed in Pile Recapitulation															
Туре	Distribution Reinforcement				Spi	iral Rei	nforce	ement	Concrete Casting Depth		Base Plate					
	Amount				Length (mm)	Amount				Length (mm)		Thickness (mm) Anchor				
Single	7	D	-	32	640	ø	12	-	75	To - 1 mLWS		10	3	-	ø	22
Batter	5	D	-	32	640	ø	12	-	75	To – 1 mLWS		10	3	-	ø	22

T-1-1- 11

Table 12.
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Forces on Retaining Wall Recapitulation							
Position	Forces	Unit					
D	Н	2591,54 kN					
breast wall	Μ	-190,67 kN.m					
Foot	Н	3239,54 Kn					
FOOL	Μ	70,68 Kn.m					
Contilouor	Н	526,38 kN					
Canthever	Μ	-55,08 kN.m					
Stiffonor	Н	185,08 kN					
Suitener	М	118,46 kN.m					

Table 13.

	Retaining Wall Reinforcement Recapitulation							
Castion	Flexural	Shear	Crack Width					
Section	Reinforcement	Reinforcement	(mm)					
Breast Wall	D25-100	D13-150	-0,041					
Foot	D19-200	D13-120	-0,716					
Cantilever	D32-150	D13-170	0.006					

D22-100

 Table 14.

 Rip – Rap Dimension Recapitulation

 Layer
 Type
 W (ton)
 Thickness (m)

 Primary
 Rock
 1,5
 1,7

 Secondary
 Rock
 0,15
 2

$$\omega_t = 1,73 \sqrt{\frac{EI}{\frac{Wl^2}{g}}} > \omega$$

#### 9) Retaining Wall Planning

Stiffener

There are 4 sections of retaining wall (breast wall, foot, cantilever, and stiffener). Reinforcement planning of retaining wall was calculated same as slab reinforcement planning.

Table 12 is recapitulation of forces on retaining wall. Retaining wall reinforcement recapitulation can be seen on Table 13.

## 10) Rip – Rap Planning

To retain the soil behind the jetty structure, a rip-rap structure is required. The structure is divided into 2 layers, primary and secondary.

Rip – rap planning is based on [1]. To control rip-rap stability, the Geo5 application is used to assist stability control. Table 14 is the dimensions of rip – rap. Rip – rap stability control can be seen on Table 15.

#### B. Construction Method

D16-120

The construction implementation method of open pier jetty Molotabu, Gorontalo, as follow:

-0,013

# 1) Preparation work

Including permission, land clearing, and keet director.

### 2) Lower Structure

Before upper structure work, lower structure needs to be done first. Lower structure work including; dredging, rip-rap work, retaining wall work, and pile installation.

## 3) Upper Structure

Upper structure works are pile cap work, beam work, and slab work.

#### 4) Fender and Bollard Installation

And the last one is jetty's facilities installation, there are fender and bollard installation.

#### C. Cost Estimating

In determining price of wages, materials, and equipment, the price chosen is from *Peraturan Menteri Perhubungan No*.

Table 15.           Bin – Ban Control Recapitulation											
Method	FS	FS min	Status								
Bishop	2,54	1,5	OK								
Fellenius/Peterson	2,21	1,5	OK								
Spencer	2,53	1,5	OK								
Janbu	2,53	1,5	OK								
Morgenstern-Prince	2,53	1,5	ОК								
C-	Table 16.										
	st Estimating Rec	apitulation									
	Cost Recapitul	ation									
No Work	Breakdown	Work I	Price								
1 Preparation Wo	ork	Rp	106.200.000								
2 Upper Structure	e Work	Rp	3.569.646.300								
3 Lower Structur	e Work	Rp	43.896.009.492								
4 Jetty Facilities	Work	Rp	3.752.401.017								
Total		Rp	51.324.256.809								
	Table 17										
]	Layout Evaluation	n Results									
T 4'	I	Result									
Location	Information	Dimensi	on Unit								
Entrance Channel	Depth	6,5	-mLWS								
Entrance Channel	Width	125	m								
Turning Pasin	Depth	6,5	-mLWS								
Turning Dasin	Diameter	194	m								
	Depth	6,5	-mLWS								
Berth Basin	Length	108	m								
	Width	50	m								
Anchorage Area	Radius	250	m								
	Length	108	m								
Jetty Dimension	Width	20	m								
	Elevation	3,5	+mLWS								
Dredging	Volume	20.300	m <sup>3</sup>								
Rip-rap	Height	3,7	m								

78 *Tahun 2014* was adjusted to prices in Gorontalo by multiplying by the expensiveness index value in Gorontalo. The recapitulation of cost estimating for open pier jetty Molotabu, Gorontalo, can be seen on Table 16.

#### IV. CONCLUSION

Based on analyzis and evaluation that have been carried out, the conclusion is as follow; (1) The result of water and land layout can be seen on Table 17; (2) The result of jetty's structure can be seen on Table 18 and Table 19; (3) Construction implementation method of this project started from dredging, rip-rap work, retaining wall work, and ended with jetty's structure work; (4) Estimated cost for this project is Rp 51.324.256.809,00 (*Fifty-one billion three hundred twenty-four million two hundred fifty-six thousand eight hundred and nine rupiah*)

#### REFERENCES

- C. T. Bishop, M. A. Donelan, and K. K. Kahma, "Shore protection manual's wave prediction reviewed," *Coast. Eng.*, vol. 17, no. 1, pp. 25–48, 1992, doi: 10.1016/0378-3839(92)90012-J.
- [2] T. Shimada, "The overseas coastal area development institute of japan (ocdi) planning division, engineering division, management & operation division, economic division," *Doboku Gakkai Ronbunshu*, vol. 1987, no. 377, pp. 15–16, 1987, ISSN:: 10.2208/jscej.1987.15.
- [3] B. S. Institution, Maritime Works Part 5 Code of Practice for

Rin	– Rap	Table Dimensi	e 18. on Reca	pitulati	on		
Layer	Туре	Dimensi	W (ton)		Thickne	ess (m)	
Primary Secondary	Rock Rock		1,5		1,7 2		
becondury	ROOK		0,10		-		
		Table	19				
	Struc	ture Plan	ning Re	sult			
Retaining Wall							
Retaining Wall Length	<b>`</b>	27	m	v	4		
Breast Wall Dimensio	n	40	v v	200	cm		
Foot Dimension		250	x	40	cm		
Cantilever Dimension		15	x	35	cm		
Stiffener Dimension		30	x	177	cm		
Concrete Ouality		f'c	35				
Concrete Cover		6			cm		
Reinforcement Quality	/	BJTP	280	&	BJTS	280	
Breast Wall Reinforce	ment	D	25				
Shear Reinforcement		ø	13	ø			
Jetty							
Structure Dimension		108	х	20	m		
Crown Height		+2,5			m LWS	5	
Concrete Cover		6			cm		
Slab Thickness		35			cm		
Beam Dimension		75	х	50	cm		
Single Pile Cap		200	х	200	х	100	cm
Batter Pile Cap		300	х	200	х	100	cm
Concrete Quality		f'c	35				
Steel Pile Quality		SKK	490				
Reinforcement Quality	/	BJTP	280	&	BJTS	280	
Slab Reinforcement		D	22	&	D	16	
Flexural Reinforcement	nt	D	19	&	D	32	
Shear Reinforcement		ø	22				
Pile		SPP	ø600				
Pile Depth		-3	s/d	-17	m LAT		
Fender		SCN 1	000 F2.7	+ Fron	tal Pad 3	,8 x 2 r	n
Bollard		Pillar E	Bollard 5	JΤ			

*Dredging and Land Reclamation*, 1st ed. London: BSI Group Headquarters, 2016. ISSN: 9780539084238.

- B. S. Institution, Maritime Works Part 1 Code of Practice for General Criteria, 1st ed. London: BSI Group Headquarters, 2000. ISSN: 0580331695.
- B. S. Institution, Maritime Works Part 1-4 General Code of Practice for Materials, 1st ed. London: BSI Group Headquarters, 2013. ISSN: 9784420899673.
- [6] B. S. Institution, Maritime Works Part 2 Code of Practice for The Design of Quay Walls, Jetties and Dolphin, 1st ed. London: BSI Group Headquarters, 2010. ISSN: 9780580984785.
- [7] Departemen Pekerjaan Umum, (PUBI) Peraturan Beton Bertulang Indonesia 1971 N.I - 2, 1st ed. Jakarta: Departemen Pekerjaan Umum, 1971. ISSN: 3591069355.
- Badan Standardisasi Nasional, Standar Nasional Indonesia. SNI-1725-2016-Pembebanan Untuk Jembatan, 1st ed. Jakarta: Badan Standardisasi Nasional, 2016.
- [9] Badan Standardisasi Nasional, Standar Nasional Indonesia. SNI-1726-2020-Tata Cara Perencanaan Ketahanan Gempa untuk Struktur Bangunan Gedung dan NonGedung, 1st ed. Jakarta: Badan Standardisasi Nasional, 2020.
- [10] Badan Standardisasi Nasional, Standar Nasional Indonesia. SNI-1727-2020-Beban Desain Minimum dan Kriteria Terkait untuk Bangunan Gedung dan Struktur Lain, 1st ed. Jakarta: Badan Standardisasi Nasional, 2020.
- [11] Badan Standarisasi Nasional, *Baja Tulangan Beton: SNI 2052:2017*, 1st ed. Jakarta: Badan Standarisasi Nasional, 2017.
- [12] Badan Standardisasi Nasional, Standar Nasional Indonesia. SNI-2052-2017-Baja Tulangan Beton, 1st ed. Jakarta: Badan Standardisasi Nasional, 2020.
- [13] PIANC, Harbour Approach Channels Design Guidelines, 1st ed. Belgique: PIANC, 2014. ISSN: 9781523103379.